

# 弹性介质的 Lagrange 动力学与地震波方程

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本文将地球介质看作是弹性介质, 从弹性体的 Navier 方程出发, 建立均匀弹性介质和非均匀弹性介质的分析动力学方程——Lagrange 方程, 利用弹性介质的 Lagrange 方程导出匀弹性介质和非均匀弹性介质的地震波方程, 为用 Lagrange 分析动力学研究地球介质中地震波传播规律和解决地震勘探中的有关问题提供基础.

**关键词:** 地震勘探, 弹性介质, Lagrange 方程, 地震波方程

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## 1 引言

地球介质可认为是弹性介质, 地震勘探中地球介质内传播的地震波是弹性波. 弹性波波动方程描述了弹性波传播的基本规律, 它是地震波动力学理论的核心, 讨论地震波动力学问题就是讨论地震波波动方程的建立和它的解, 以及由此得出的结论在地震勘探中的应用. 以地震波动力学为基础, 发展出的地球物理勘探技术, 在油气地震勘探中有着广泛应用, 如波动方程的正演模拟技术、波动方程地震偏移技术, 以及基于波动方程的反演技术等. 无论正、反演理论的建立, 还是地震勘探技术的实际应用, 波动方程的地位都极为重要.

在实际中, 地震勘探处理的介质通常是具有复杂结构的非均匀地球介质, 地震波场在这些介质中传播过程非常复杂. 利用分析力学理论处理复杂系统问题更具优越性, 随着计算机技术的飞速发展, 对于复杂工程对象的动力学计算已经愈来愈多的使用分析力学的方法. 近些年, 国内外学者在 Lagrange 体系、Hamilton 体系、Birkhoff 体系分析动力学和对称性与守恒量理论研究方面取得了许多成果<sup>[1-12]</sup>, 笔者试图将其用于研究地震波动力学问题, 期望能用分析动力学理论和方法处理

和解决地震勘探中的一些问题. 文献 [13, 14] 基于 Hamilton 分析力学理论, 研究了地震勘探中地震波传播的 Hamilton 表述、共反射点轨迹、辛几何算法等. 本文将地球介质看成弹性介质, 从弹性体的 Navier 方程出发, 建立均匀弹性介质和非均匀弹性介质的 Lagrange 方程, 利用弹性介质的 Lagrange 方程导出匀弹性介质和非均匀弹性介质的地震波方程, 为用 Lagrange 分析动力学研究地球介质中地震波传播、处理和解决地震勘探中的有关问题提供基础.

Lagrange 力学和 Hamilton 力学是分析力学的两种表示形式, 这两种不同数学形式陈述同一物理规律, Lagrange 体系将力学系统表示为一个变分极值问题, Hamilton 体系则给出在相空间 (位置和动量) 的一阶微分方程. 由于形式不同, 它们在实践中对解决问题会提供不同的途径, 因此等价的数学形式在实践中可能是不等效的. 当将它们表示成数值算法时, 计算过程是不同的, Lagrange 体系表述下的算法是有限元方法, Hamilton 表述下的算法是辛几何算法. 地震波传播过程, 本质上是能量在地球介质中传播并逐步损耗直至殆尽的过程, 但在实际应用中, 一旦把地震波传播用弹性波动方程或标量波动方程描述时, 都采用了无能量损耗的假设. 在

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Lagrange 体系下和 Hamilton 体系下描述地震波, 导出各种介质的地震波方程, 将为利用分析力学的理论和方法研究地球介质中地震波的传播、讨论和处理有关地震勘探问题奠定基础.

## 2 弹性介质的 Lagrange 方程

地震勘探中地球介质常被看作弹性介质, 下面建立弹性介质的 Lagrange 方程, 以使用 Lagrange 分析力学理论和方法研究处理地震波传播的有关问题.

### 2.1 弹性体的 Navier 方程

弹性介质中质点的位置矢量在直角坐标系中表示为

$$\mathbf{r} = xi + yj + zk, \quad (1)$$

质点的位移矢量为

$$\mathbf{u} = ui + vj + wk. \quad (2)$$

质点位置是在其静止状态下定义的, 位置坐标  $x, y, z$  不随时间  $t$  变化, 不同位置的质点其位移不同, 位移是位置坐标和时间的函数, 即  $\mathbf{u} = \mathbf{u}(x, y, z, t)$ .

利用牛顿第二定律, 可建立弹性介质中单位体元的运动微分方程, 即 Navier 方程为<sup>[15]</sup>

$$\begin{aligned} \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} + F_x &= \rho \frac{\partial^2 u}{\partial t^2}, \\ \frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} + F_y &= \rho \frac{\partial^2 v}{\partial t^2}, \\ \frac{\partial \sigma_{zx}}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + F_z &= \rho \frac{\partial^2 w}{\partial t^2}, \end{aligned} \quad (3)$$

式中  $\rho$  为弹性介质的密度,  $\sigma$  为应力,  $F$  为体力. 按照爱因斯坦求和约定, (3) 式可简写为

$$\frac{\partial \sigma_{ij}}{\partial x_j} + F_i = \rho \frac{\partial^2 u_i}{\partial t^2}, \quad (4)$$

式中  $i, j = 1, 2, 3$ , 分别表示  $x, y, z$ . 利用逗号约定, 上式可写为

$$\sigma_{i,j,j} + F_i = \rho u_{i,tt}. \quad (5)$$

### 2.2 均匀弹性介质的 Lagrange 方程

按照分析力学理论<sup>[16]</sup>, 在完整理想约束下, 如果选取  $n$  个广义坐标  $q_s (s = 1, 2, \dots, n)$ , 这里

$q_s = q_s(x, y, z, t)$ , 则  $u_i$  可表示为

$$u_i = u_i(q_s, x, y, z, t), \quad (i = 1, 2, 3; s = 1, \dots, n), \quad (6)$$

(6) 式中的  $x, y, z$  是与  $t$  等同的参量. 于是有

$$\begin{aligned} du_i &= \frac{\partial u_i}{\partial q_1} dq_1 + \dots + \frac{\partial u_i}{\partial q_n} dq_n + \frac{\partial u_i}{\partial x} dx \\ &\quad + \frac{\partial u_i}{\partial y} dy + \frac{\partial u_i}{\partial z} dz + \frac{\partial u_i}{\partial t} dt \\ &= \frac{\partial u_i}{\partial q_s} dq_s + \frac{\partial u_i}{\partial x_v} dx_v, \end{aligned} \quad (7)$$

式中  $v = 1, 2, 3, 4$ , 分别表示  $x, y, z, t$ . 以  $\delta u_i$  表示等参量变分 (这时  $\delta x_v = 0$ ), 即虚位移, 则有

$$\delta u_i = \frac{\partial u_i}{\partial q_s} \delta q_s. \quad (8)$$

将 (5) 式右端的项移到左端后乘以  $\delta u_i$ , 并利用 (8) 式, 有

$$\left( \sigma_{ij,j} \frac{\partial u_i}{\partial q_s} + Q_s - \rho u_{i,tt} \frac{\partial u_i}{\partial q_s} \right) \delta q_s = 0, \quad (9)$$

其中

$$Q_s = F_i \frac{\partial u_i}{\partial q_s}, \quad (10)$$

为广义体力. 在理想约束下式 (10) 中的  $F_i$  仅指主动体力.

$$\begin{aligned} &\rho u_{i,tt} \frac{\partial u_i}{\partial q_s} \\ &= \rho \frac{\partial}{\partial t} \left( u_{i,t} \frac{\partial u_i}{\partial q_s} \right) - \rho \frac{\partial}{\partial q_s} \left( \frac{1}{2} u_{i,t} u_{i,t} \right), \end{aligned} \quad (11)$$

由 (6) 式可知

$$\frac{\partial u_i}{\partial t} = \frac{\partial u_i}{\partial q_s} \frac{\partial q_s}{\partial t} + \frac{Du_i}{Dt}, \quad (12)$$

式中  $\frac{\partial u_i}{\partial t}$  表示  $u_i$  中的  $x, y, z$  不变时对  $t$  的偏导数,  $\frac{Du_i}{Dt}$  表示  $u_i$  中的  $q_s, x, y, z$  不变时对  $t$  的偏导数. 注意到  $\frac{\partial u_i}{\partial q_s}$  和  $\frac{Du_i}{Dt}$  中不含  $q_{s,t}$ , 由 (12) 式可求得

$$\frac{\partial u_{i,t}}{\partial q_{s,t}} = \frac{\partial u_i}{\partial q_s}. \quad (13)$$

类似的有

$$\frac{\partial u_{i,j}}{\partial q_{s,j}} = \frac{\partial u_i}{\partial q_s}. \quad (14)$$

将 (13) 式代入 (11) 式, 有

$$\begin{aligned} \rho u_{i,tt} \frac{\partial u_i}{\partial q_s} &= \rho \frac{\partial}{\partial t} \left[ \frac{\partial}{\partial q_{s,t}} \left( \frac{1}{2} u_{i,t} u_{i,t} \right) \right] \\ &\quad - \rho \frac{\partial}{\partial q_s} \left( \frac{1}{2} u_{i,t} u_{i,t} \right). \end{aligned} \quad (15)$$

对于均匀弹性介质,  $\rho$  为常量, 故有

$$\rho u_{i,t} \frac{\partial u_i}{\partial q_s} = \frac{\partial}{\partial t} \frac{\partial T}{\partial q_{s,t}} - \frac{\partial T}{\partial q_s}, \quad (16)$$

式中  $T = \frac{1}{2} \rho u_{i,t} u_{i,t}$  为单位弹性体的动能, 即弹性体的动能密度.

$$\begin{aligned} \sigma_{ij,j} \frac{\partial u_i}{\partial q_s} &= \frac{\partial \sigma_{ij}}{\partial x_j} \frac{\partial u_i}{\partial q_s} \\ &= \frac{\partial}{\partial x_j} \left( \sigma_{ij} \frac{\partial u_i}{\partial q_s} \right) - \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_s}, \end{aligned} \quad (17)$$

注意到 (14) 式, 有

$$\begin{aligned} \sigma_{ij,j} \frac{\partial u_i}{\partial q_s} &= \frac{\partial}{\partial x_j} \left( \sigma_{ij} \frac{\partial u_{i,k}}{\partial q_{s,k}} \right) \\ &\quad - \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_s} \quad (k = 1, 2, 3). \end{aligned} \quad (18)$$

弹性介质的应变能密度为<sup>[17]</sup>

$$U = \frac{1}{2} \sigma_{ij} e_{ij} = \frac{1}{2} C_{ijkl} e_{ij} e_{kl}, \quad (19)$$

式中  $\sigma_{ij} = C_{ijkl} e_{kl}$ ,  $e_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i})$ ,  $C_{ijkl}$  为弹性系数. 对于均匀弹性介质,  $C_{ijkl}$  为常数, 于是有

$$\begin{aligned} \frac{\partial U}{\partial q_s} &= \frac{1}{2} \left( C_{ijkl} e_{ij} \frac{\partial e_{kl}}{\partial q_s} + C_{ijkl} e_{kl} \frac{\partial e_{ij}}{\partial q_s} \right) \\ &= \frac{1}{2} \left( \sigma_{kl} \frac{\partial e_{kl}}{\partial q_s} + \sigma_{ij} \frac{\partial e_{ij}}{\partial q_s} \right) \\ &= \frac{1}{2} \left\{ \sigma_{kl} \frac{\partial}{\partial q_s} \left[ \frac{1}{2}(u_{k,l} + u_{l,k}) \right] \right. \\ &\quad \left. + \sigma_{ij} \frac{\partial}{\partial q_s} \left[ \frac{1}{2}(u_{i,j} + u_{j,i}) \right] \right\} \\ &= \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_s}. \end{aligned} \quad (20)$$

同理, 可得

$$\frac{\partial U}{\partial q_{s,k}} = \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_{s,k}}, \quad (21)$$

而

$$\begin{aligned} \frac{\partial}{\partial x_j} \left( \sigma_{ij} \frac{\partial u_{i,k}}{\partial q_{s,k}} \right) &= \frac{\partial}{\partial x_k} \left( \sigma_{ik} \frac{\partial u_{i,k}}{\partial q_{s,k}} \right) \\ &= \frac{\partial}{\partial x_k} \left( \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_{s,k}} \right) \\ &= \frac{\partial}{\partial x_k} \frac{\partial U}{\partial q_{s,k}}. \end{aligned} \quad (22)$$

将 (20) 式和 (22) 式代入 (18) 式, 得

$$\sigma_{ij,j} \frac{\partial u_i}{\partial q_s} = \frac{\partial}{\partial x_k} \frac{\partial U}{\partial q_{s,k}} - \frac{\partial U}{\partial q_s}. \quad (23)$$

将 (16) 式和 (23) 式代入 (9) 式, 得

$$\left( \frac{\partial}{\partial x_j} \frac{\partial U}{\partial q_{s,k}} - \frac{\partial U}{\partial q_s} - \frac{\partial}{\partial t} \frac{\partial T}{\partial q_{s,t}} + \frac{\partial T}{\partial q_s} + Q_s \right) \delta q_s$$

$$= 0, \quad (24)$$

考虑到  $T$  中不显含  $q_{s,k}$ ,  $U$  中不显含  $q_{s,t}$ , (24) 式可进一步写为

$$\left( -\frac{\partial}{\partial x_v} \frac{\partial L}{\partial q_{s,v}} + \frac{\partial L}{\partial q_s} + Q_s \right) \delta q_s = 0, \quad (25)$$

其中  $L = T - U$  为 Lagrange 密度函数. 注意到  $\delta q_s$  的独立性, 得均匀弹性介质的 Lagrange 方程

$$\frac{\partial}{\partial x_v} \frac{\partial L}{\partial q_{s,v}} - \frac{\partial L}{\partial q_s} = Q_s. \quad (26)$$

如果  $F_i$  中有保守力, 与其相应的势能密度为  $V$ , 则 (26) 式可表示为

$$\frac{\partial}{\partial x_v} \frac{\partial \bar{L}}{\partial q_{s,v}} - \frac{\partial \bar{L}}{\partial q_s} = \bar{Q}_s, \quad (27)$$

式中的 Lagrange 密度函数  $\bar{L} = T - U - V$ ,  $\bar{Q}_s$  为非势广义体力.

### 2.3 非均匀弹性介质的 Lagrange 方程

对于非均匀弹性介质, 一般的情况是  $\rho = \rho(q_s, q_{s,v}, x_v)$ ,  $C_{ijkl} = C_{ijkl}(q_s, q_{s,v}, x_v)$ , 于是有

$$\begin{aligned} \rho u_{i,t} \frac{\partial u_i}{\partial q_s} &= \rho \frac{\partial}{\partial t} (u_{i,t} \frac{\partial u_{i,t}}{\partial q_{s,t}}) - \rho \frac{\partial}{\partial q_s} \left( \frac{1}{2} u_{i,t} u_{i,t} \right) \\ &= \frac{\partial}{\partial t} \left[ \frac{\partial}{\partial q_{s,t}} \left( \frac{1}{2} \rho u_{i,t} u_{i,t} \right) \right] \\ &\quad - \frac{\partial \rho}{\partial t} \frac{\partial}{\partial q_{s,t}} \left( \frac{1}{2} u_{i,t} u_{i,t} \right) \\ &\quad - \frac{\partial}{\partial t} \left( \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_{s,t}} \right) \\ &\quad - \frac{\partial}{\partial q_s} \left( \frac{1}{2} \rho u_{i,t} u_{i,t} \right) + \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_s} \\ &= \frac{\partial}{\partial t} \frac{\partial T}{\partial q_{s,t}} - \frac{\partial T}{\partial q_s} - P_s, \end{aligned} \quad (28)$$

其中

$$\begin{aligned} P_s &= \frac{\partial \rho}{\partial t} \frac{\partial}{\partial q_{s,t}} \left( \frac{1}{2} u_{i,t} u_{i,t} \right) - \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_s} \\ &\quad + \frac{\partial}{\partial t} \left( \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_{s,t}} \right) \\ &= \frac{\partial \rho}{\partial t} u_{i,t} \frac{\partial u_i}{\partial q_s} - \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_s} \\ &\quad + \frac{\partial}{\partial t} \left( \frac{1}{2} u_{i,t} u_{i,t} \frac{\partial \rho}{\partial q_{s,t}} \right). \end{aligned} \quad (29)$$

而

$$\frac{\partial U}{\partial q_s} = \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_s} + \frac{1}{2} \frac{\partial C_{ijkl}}{\partial q_s} e_{ij} e_{kl}, \quad (30)$$

$$\frac{\partial U}{\partial q_{s,k}} = \sigma_{ij} \frac{\partial u_{i,j}}{\partial q_{s,k}} + \frac{1}{2} \frac{\partial C_{ijkl}}{\partial q_{s,k}} e_{ij} e_{kl}, \quad (31)$$

则

$$\sigma_{ij,j} \frac{\partial u_i}{\partial q_s} = \frac{\partial}{\partial x_k} \frac{\partial U}{\partial q_{s,k}} - \frac{\partial U}{\partial q_s} + M_s, \quad (32)$$

其中

$$M_s = \frac{1}{2} \frac{\partial C_{ijkl}}{\partial q_s} e_{ij} e_{kl} - \frac{1}{2} \frac{\partial}{\partial x_k} \left( \frac{\partial C_{ijkl}}{\partial q_{s,k}} e_{ij} e_{kl} \right). \quad (33)$$

类似于前面的讨论, 可得非均匀弹性介质的 Lagrange 方程为

$$\frac{\partial}{\partial x_v} \frac{\partial L}{\partial q_{s,v}} - \frac{\partial L}{\partial q_s} = Q_s + P_s + M_s, \quad (34)$$

和

$$\frac{\partial}{\partial x_v} \frac{\partial \bar{L}}{\partial q_{s,v}} - \frac{\partial \bar{L}}{\partial q_s} = \bar{Q}_s + P_s + M_s. \quad (35)$$

在实际中, 一般认为  $\rho, C_{ijkl}$  是空间位置的函数, 即  $\rho = \rho(x_i), C_{ijkl} = C_{ijkl}(x_i)$ , 在这种情况下,  $P_s = 0, M_s = 0$ , 方程 (34), (35) 分别化为方程 (26), (27). 可见对  $\rho, C_{ijkl}$  仅与空间位置有关的非均匀弹性介质, 其 Lagrange 方程与均匀弹性介质的 Lagrange 方程相同.

### 3 各向同性弹性介质的地震波方程

地震波方程在地震勘探中占有非常重要的地位, 现利用弹性介质的 Lagrange 方程建立弹性介质的地震波方程.

#### 3.1 均匀各向同性弹性介质的地震波方程

对各向同性弹性介质, 有<sup>[17]</sup>

$$U = \frac{1}{2} \lambda e_{kk} e_{ii} + \mu e_{ij} e_{ij} = \frac{1}{2} \lambda (e_{xx} + e_{yy} + e_{zz})^2 + \mu (e_{xx}^2 + e_{yy}^2 + e_{zz}^2) + 2\mu (e_{xy}^2 + e_{yz}^2 + e_{zx}^2), \quad (36)$$

式中  $\lambda, \mu$  为拉梅系数. 则

$$L = T - U = \frac{1}{2} \rho \left[ \left( \frac{\partial u}{\partial t} \right)^2 + \left( \frac{\partial v}{\partial t} \right)^2 + \left( \frac{\partial w}{\partial t} \right)^2 \right] - \frac{1}{2} \lambda \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)^2 - \mu \left[ \left( \frac{\partial u}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial y} \right)^2 + \left( \frac{\partial w}{\partial z} \right)^2 \right] - \frac{1}{2} \mu \left[ \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)^2 + \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right)^2 \right]. \quad (37)$$

对均匀各向同性弹性介质,  $\rho, \lambda, \mu$  均为常数, 将  $L$  代入 Lagrange 方程 (26), 注意到广义坐标  $q_1 = u, q_2 = v, q_3 = w$ , 则对  $s = 1$ , 即  $u$  分量有

$$\frac{\partial}{\partial t} \left( \rho \frac{\partial u}{\partial t} \right) - \frac{\partial}{\partial x} \left[ \lambda \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) + 2\mu \frac{\partial u}{\partial x} \right] - \frac{\partial}{\partial y} \left[ \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \right] - \frac{\partial}{\partial z} \left[ \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right] = F_x, \quad (38)$$

$$\rho \frac{\partial^2 u}{\partial t^2} - \lambda \frac{\partial}{\partial x} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) - \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) - \mu \frac{\partial}{\partial x} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) = F_x, \quad (39)$$

即

$$(\lambda + \mu) \frac{\partial \theta}{\partial x} + \mu \nabla^2 u + F_x = \rho \frac{\partial^2 u}{\partial t^2}, \quad (40)$$

其中

$$\theta = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = \nabla \cdot \mathbf{u},$$

$$\nabla = \frac{\partial}{\partial x} \mathbf{i} + \frac{\partial}{\partial y} \mathbf{j} + \frac{\partial}{\partial z} \mathbf{k},$$

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}.$$

同理, 对  $s = 2, 3$ , 即  $v, w$  分量有

$$(\lambda + \mu) \frac{\partial \theta}{\partial y} + \mu \nabla^2 v + F_y = \rho \frac{\partial^2 v}{\partial t^2}, \quad (41)$$

$$(\lambda + \mu) \frac{\partial \theta}{\partial z} + \mu \nabla^2 w + F_z = \rho \frac{\partial^2 w}{\partial t^2}. \quad (42)$$

将上述三个分量式合并成矢量式, 有

$$(\lambda + \mu) \nabla (\nabla \cdot \mathbf{u}) + \mu \nabla^2 \mathbf{u} + \mathbf{F} = \rho \frac{\partial^2 \mathbf{u}}{\partial t^2}. \quad (43)$$

上式就是均匀各向同性弹性介质的地震波方程.

#### 3.2 非均匀各向同性弹性介质的地震波方程

对非均匀各向同性弹性介质, 假设  $\rho, \lambda, \mu, C_{ijkl}$  是空间位置的函数, 即  $\rho = \rho(x_i), \lambda = \lambda(x_i), \mu = \mu(x_i), C_{ijkl} = C_{ijkl}(x_i)$ , 将  $L$  代入 Lagrange 方程 (34), 注意到广义坐标  $q_1 = u, q_2 = v, q_3 = w$ , 则对  $s = 1$ , 即  $u$  分量有

$$\frac{\partial}{\partial t} \left( \rho \frac{\partial u}{\partial t} \right) - \frac{\partial}{\partial x} \left[ \lambda \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) + 2\mu \frac{\partial u}{\partial x} \right]$$

$$-\frac{\partial}{\partial y} \left[ \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \right] - \frac{\partial}{\partial z} \left[ \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right]$$

$$=F_x, \tag{44}$$

$$\rho \frac{\partial^2 u}{\partial t^2} - (\lambda + \mu) \frac{\partial}{\partial x} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

$$- \frac{\partial \lambda}{\partial x} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) - \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$$- 2 \frac{\partial \mu}{\partial x} \frac{\partial u}{\partial x} - \frac{\partial \mu}{\partial y} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) - \frac{\partial \mu}{\partial z} \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)$$

$$=F_x, \tag{45}$$

即

$$(\lambda + \mu) \frac{\partial \theta}{\partial x} + \mu \nabla^2 u + \frac{\partial \lambda}{\partial x} \theta + 2 \frac{\partial \mu}{\partial x} \frac{\partial u}{\partial x}$$

$$+ \frac{\partial \mu}{\partial y} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) + \frac{\partial \mu}{\partial z} \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) + F_x$$

$$= \rho \frac{\partial^2 u}{\partial t^2}. \tag{46}$$

同理, 对  $s = 2, 3$ , 即  $v, w$  分量有

$$(\lambda + \mu) \frac{\partial \theta}{\partial y} + \mu \nabla^2 v + \frac{\partial \lambda}{\partial y} \theta + 2 \frac{\partial \mu}{\partial y} \frac{\partial v}{\partial y}$$

$$+ \frac{\partial \mu}{\partial x} \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) + \frac{\partial \mu}{\partial z} \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) + F_y$$

$$= \rho \frac{\partial^2 v}{\partial t^2}, \tag{47}$$

$$(\lambda + \mu) \frac{\partial \theta}{\partial z} + \mu \nabla^2 w + \frac{\partial \lambda}{\partial z} \theta + 2 \frac{\partial \mu}{\partial z} \frac{\partial w}{\partial z}$$

$$+ \frac{\partial \mu}{\partial x} \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) + \frac{\partial \mu}{\partial y} \left( \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) + F_z$$

$$= \rho \frac{\partial^2 w}{\partial t^2}. \tag{48}$$

将上述三个分量式合并成矢量式, 有

$$(\lambda + \mu) \nabla (\nabla \cdot \mathbf{u}) + \mu \nabla^2 \mathbf{u} + \nabla \lambda \nabla \cdot \mathbf{u}$$

$$+ \frac{\partial \mu}{\partial x} \left( \nabla u + \frac{\partial \mathbf{u}}{\partial x} \right) + \frac{\partial \mu}{\partial y} \left( \nabla v + \frac{\partial \mathbf{u}}{\partial y} \right)$$

$$+ \frac{\partial \mu}{\partial z} \left( \nabla w + \frac{\partial \mathbf{u}}{\partial z} \right) + \mathbf{F} = \rho \frac{\partial^2 \mathbf{u}}{\partial t^2}. \tag{49}$$

上式就是非均匀各向同性弹性介质的地震波方程.

## 4 结论

在将地球介质看作是弹性介质的情况下, 从弹性体的 Navier 方程出发, 用分析力学方法建立了均匀弹性介质的 Lagrange 方程和非均匀弹性介质的 Lagrange 方程, 由弹性介质的 Lagrange 方程导出了均匀弹性介质和非均匀弹性介质的地震波方程. 本文结果为用 Lagrange 分析动力学研究地球介质中地震波传播、处理和解决地震勘探中的有关问题提供了基础.

如果在分析力学体系 (Lagrange 体系、Hamilton 体系等) 下描述地震波, 导出或建立各种介质的地震波方程, 得到描述地震波的量与分析力学量间的联系, 则可利用分析力学的理论和方法研究地震波的传播、讨论各种介质中地震波的求解、处理和解决地震勘探的有关问题.

[1] Mei F X 2004 *Symmetries and Conserved Quantities of Constrained Mechanical Systems* (Beijing: Beijing Institute of Technology Press) (in Chinese) [梅凤翔 2004 约束力学系统的对称性与守恒量 (北京: 北京理工大学出版社)]

[2] Chen X W, Zhang R C, Mei F X 2000 *Acta Mech. Sin.* **16** 282

[3] Fu J L, Chen L Q 2004 *Mech. Res. Commun.* **31** 9

[4] Luo S K, Chen X W, Guo Y X 2007 *Chin. Phys.* **16** 3176

[5] Luo S K, Zhang Y F 2008 *Advances in the Study of Dynamics of Constrained System* (Beijing: Science Press) (in Chinese) [罗绍凯, 张永发 2008 约束系统动力学研究进展 (北京: 科学出版社)]

[6] Mei F X, Wu H B 2008 *Phys. Lett. A* **372** 2141

[7] Zhang Y 2009 *Acta Phys. Sin.* **58** 7436 (in Chinese) [张毅 2009 物理学报 **58** 7436]

[8] Dorodnitsyn V, Kozlov R 2010 *J. Eng. Math.* **66** 235

[9] Nucci M C 2011 *Phys. Lett. A* **375** 1375

[10] Jia L Q, Xie Y L, Luo S K 2011 *Acta Phys. Sin.* **60** 040201 (in Chinese) [贾利群, 解银丽, 罗绍凯 2011 物理学报 **60** 040201]

[11] Cai J L, Shi S S 2012 *Acta Phys. Sin.* **61** 030201 (in Chinese) [蔡建乐, 史生水 2012 物理学报 **61** 030201]

[12] Ge W K, Zhang Y, Lou Z M 2012 *Acta Phys. Sin.* **61** 140204 (in Chinese) [葛伟宽, 张毅, 楼智美 2012 物理学报 **61** 140204]

[13] Liu H, Luo M Q, Li Y M, Yang K Q 1999 *Chin. J. Geophys.* **42** 685 (in Chinese) [刘洪, 罗明秋, 李幼铭, 杨孔庆 1999 地球物理学报 **42** 685]

[14] Luo M Q, Liu H, Li Y M 2001 *Chin. J. Geophys.* **44** 210 (in Chinese) [罗明秋, 刘洪, 李幼铭 2001 地球物理学报 **44** 210]

[15] Sun C Y 2007 *Theory and Methods of Seismic Waves* (dongying: China University of Petroleum Press) (in Chinese) [孙成禹 2007 地震波理论与方法 (东营: 中国石油大学出版社)]

[16] Mei F X, Liu D, Luo Y 1993 *Advanced Analytical Mechanics* (Beijing: Beijing Institute of Technology Press) (in Chinese) [梅凤翔, 刘端, 罗勇 1993 高等分析力学 (北京: 北京理工大学出版社)]

[17] Zhu B 2008 *Elastic Mechanics* (Hefei: University of Science and Technology of China Press) (in Chinese) [朱滨 2008 弹性力学 (合肥: 中国科学技术大学出版社)]

# Lagrangian dynamics and seismic wave align of elastic medium

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## Abstract

In seismic exploration, propagation of seismic wave in earth medium is very complex. Theory of analytical mechanics has advantages for solving complicated problems. In this paper, with the hypothesis of viewing geological medium as an elastic medium, the Lagrange equations of analytical dynamics are built for homogeneous and inhomogeneous earth media. Then the seismic wave equations of elastic medium are obtained from the Lagrange equations. The results provide the basis to study propagation of seismic wave in earth medium and discuss problems related to seismic exploration using Lagrange analytic dynamics.

**Keywords:** seismic exploration, elastic medium, Lagrange equation, seismic wave equation

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