

通过注入激光提高腔内参量 放大光的压缩*

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本文将证明采用注入激光以弥补腔内损耗, 减少无规力的作用, 可以获得很高的腔内参量放大光的压缩.

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一、引 言

早期的简并参量放大产生压缩态光的理论^[1], 就已经得出“当计及光的损耗时, 最多只能有 2 倍的压缩”. 后来 Yurke 引进谐振腔的作用后^[2], 认为可通过选择谐振腔参数, 使得在阈值附近工作时, 输出光的压缩可趋于很大. 但在 Yurke 的讨论中, 已完全略去阻尼, 也略去伴随阻尼而来的无规力的作用. 其实无阻尼的简并四波混频产生压缩态的研究^[3,4]表明, 只要相互作用路程够长(这可通过谐振腔来解决), 可增大光的压缩而不受限制. 稍后, Collett 的研究又表明^[5], 在对输出压缩光作了谱分析后, 得出

$$:S_{2,\text{out}}(\omega): = -\frac{r_1}{4} \frac{r_1 + r_2}{(r_1 + r_2)^2 + \omega^2}.$$

当 $r_2 = 0$, $\omega \rightarrow 0$ 时

$$:S_{2,\text{out}}(0): = -\frac{1}{4}$$

但总的输出光的压缩仍为

$$:S_{2,\text{out}}: = \frac{1}{2\pi} \int -\frac{r_1}{4} \frac{r_1^2}{r_1^2 + \omega^2} \delta(\omega + \omega') d\omega d\omega' = -\frac{r_1}{8}.$$

即有 2 倍压缩的光乘上透过率输出 r_1 . 如果在腔外加滤光片将 $\omega = 0$ 分量的光分离出来, 可达理想的压缩, 否则仍为腔内的 2 倍压缩. 后来又有简并参量放大压缩光信噪比计算^[6], 实际上正如他自己指出的^[7], 是用极限 $(r/2 - \epsilon)T \gg 1$, 即假定探测器宽度远小于参量放大输出的谱宽. 这与外加滤光片将 $\omega = 0$ 分量的光分离出来有同样效果. 但要求光探测器探测时间 T 远大于压缩光信号的相干时间.

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本文将证明通过由腔外注入相干光的方法,可抵偿腔的输出等损耗以及由此而来的无规力的影响,从而得到在阈值附近的腔内理想压缩,即腔内压缩可以很大。

二、有相干光注入的多模参量放大方程及其解

设参量放大腔的模式频率为 $\omega_0/2$, 而光泵频率为 ω_p , 并设光泵频率已调谐到 $\omega_p = 2(\omega_0/2) = \omega_0$, 如果注入光 a_{in} 的频率又恰好为 $\omega_0/2$, 于是在输入的信号光的作用下, 一个频率为 ω_0 的泵浦光子, 简并参量转换为两个频率为 $\omega_0/2$ 的光子。若信号光的频率为 $\omega_0/2 \pm \omega$, 则频率为 ω_0 的泵浦光, 参量转换为频率分别为 $\omega_0/2 + \omega, \omega_0/2 - \omega$ 的两个光子。与前一种单模简并参量转换形成对比, 这就是多模参量转换的情形。设参量光的湮没与产生算符为 a 与 a^+ 。则参照文献[8], 关于算符 a 的量子 Langevan 方程可写为

$$\frac{da}{dt} = -i/\hbar[a, H] - x/2a + F. \quad (1)$$

式中 $-x/2a$ 为阻尼项, F 为无规力项, 表现与热库的相互作用。而 H 即系统的 Hamilton 可表示为振荡的场能、简并参量能^[6]与注入激光能^[9]之和。

$$\begin{aligned} H = & \frac{\hbar\omega_0}{2} a^+a + \frac{i\hbar}{2} [\epsilon \exp(-i\omega_0 t)(a^+)^2 - \epsilon^* \exp(i\omega_0 t)a^2] \\ & + K[a^+a_{in} - a_{in}^+a] + \frac{\hbar\omega_0}{2} a_{in}^+a_{in} \\ K = & T \left(\frac{\omega_0 \epsilon_0}{2\hbar V} \right)^{1/2} \bar{x}/2, \end{aligned} \quad (2)$$

$$\begin{aligned} a_{in} = & \frac{1}{\sqrt{2}} (a_{in}(\omega) \exp[-i(\omega_0/2 + \omega)t] + a_{in}(-\omega) \exp[-i(\omega_0/2 - \omega)t]), \\ a_{in}^+ = & \frac{1}{\sqrt{2}} (a_{in}^+(\omega) \exp[i(\omega_0/2 + \omega)t] + a_{in}^+(-\omega) \exp[i(\omega_0/2 - \omega)t]). \end{aligned} \quad (2')$$

式中 ϵ 为描述参量放大的非线性系数。若 $\epsilon = |\epsilon| \exp(i\phi)$, 则可通过变换 $a \rightarrow a \exp(i\phi/2), a^+ \rightarrow a^+ \exp(-i\phi/2), a_{in} \rightarrow a_{in} \exp(i\phi/2), a_{in}^+ \rightarrow a_{in}^+ \exp(-i\phi/2)$, 将相角消掉。故不失一般性, 将 ϵ 取为实数。由(2)式定义的 K 称为注入激光的注入率。其中 \bar{x} 为激光媒质的极化率。 V 为腔的体积。 T 为腔端面的透射系数。(2)'式表明注入激光包含 $\omega_0/2 \pm \omega$ 两个频率。

将(2)式代入(1)式, 则得参量放大的 Langevan 方程

$$\frac{da}{dt} = (-i\omega_0/2 - x)a + \epsilon \exp(-i\omega_0 t)a^+ + Ka_{in} + F. \quad (3)$$

同样可得

$$\frac{da^+}{dt} = (i\omega_0/2 - x)a^+ + \epsilon \exp(i\omega_0 t)a + Ka_{in}^+ + F^+. \quad (3)'$$

作旋转坐标变换

$$\begin{aligned} a &\rightarrow a \exp(-i\omega_0/2)t, & a^+ &\rightarrow a^+ \exp(i\omega_0/2)t, \\ F &\rightarrow F \exp(-i\omega_0/2)t, & F^+ &\rightarrow F^+ \exp(i\omega_0/2)t. \end{aligned} \quad (4)$$

并注意到(2)'式, 则得

$$\begin{aligned} \frac{da}{dt} &= -\kappa a + \epsilon a^+ + \frac{K}{\sqrt{2}} (a_{in}(\omega) \exp(-i\omega t) + a_{in}(-\omega) \exp(i\omega t)) + F, \\ \frac{da^+}{dt} &= -\kappa a^+ + \epsilon a + \frac{K}{\sqrt{2}} (a_{in}^+(\omega) \exp(i\omega t) + a_{in}^+(-\omega) \exp(-i\omega t)) + F^+. \end{aligned} \quad (5)$$

为求参量放大方程(5)的解, 宜于再作一次变换, 即定义算子 b_1, b_2

$$\begin{aligned} b_1 &= \frac{a + a^+}{\sqrt{2}}, & b_2 &= \frac{a - a^+}{\sqrt{2}}, \\ b_{1i}(\omega) &= \frac{1}{\sqrt{2}} (a_{in}(\omega) + a_{in}^+(-\omega)), \\ b_{2i}(\omega) &= \frac{1}{\sqrt{2}} (a_{in}(\omega) - a_{in}^+(-\omega)), \\ G_1 &= \frac{F + F^+}{\sqrt{2}}, & G_2 &= \frac{F - F^+}{\sqrt{2}}. \end{aligned} \quad (6)$$

由(6)式易于证明

$$\begin{aligned} \langle [b_2, b_1] \rangle &= \langle b_2 b_1 - b_1 b_2 \rangle = \langle a a^+ - a^+ a \rangle = \langle [a, a^+] \rangle = 1, \\ [b_{2i}(\omega), b_{1i}(-\omega)] &= b_{2i}(\omega) b_{1i}(-\omega) - b_{1i}(-\omega) b_{2i}(\omega) \\ &= \frac{1}{2} [a_{in}(\omega) a_{in}^+(\omega) - a_{in}^+(\omega) a_{in}(\omega) \\ &\quad - a_{in}^+(-\omega) a_{in}(-\omega) + a_{in}(-\omega) a_{in}^+(-\omega)] \\ &= 1. \end{aligned} \quad (7)$$

于是由(5), (6)式便得

$$\begin{aligned} \frac{db_1}{dt} &= (-\kappa + \epsilon) b_1 + K \frac{b_{1i}(\omega) \exp(-i\omega t) + b_{1i}(-\omega) \exp(i\omega t)}{\sqrt{2}} + G_1, \\ \frac{db_2}{dt} &= (-\kappa - \epsilon) b_2 + K \frac{b_{2i}(\omega) \exp(-i\omega t) + b_{2i}(-\omega) \exp(i\omega t)}{\sqrt{2}} + G_2. \end{aligned} \quad (9)$$

令 $\lambda_1 = \kappa - \epsilon$, $\lambda_2 = \kappa + \epsilon$, (9)式可写为

$$\frac{db_j}{dt} = -\lambda_j b_j + K \frac{b_{ji}(\omega) \exp(-i\omega t) + b_{ji}(-\omega) \exp(i\omega t)}{\sqrt{2}} + G_j \quad j = 1, 2. \quad (10)$$

当注入率 $K = 0$, 则(10)式的解可参照文献[10—12]求得, 其无规力 G_1, G_2 满足如下关系:

$$\begin{aligned} \langle G_2(t) G_1(t') - G_1(t) G_2(t') \rangle &= 2\kappa \delta(t - t'), \\ \langle :G_1(t) G_1(t') : \rangle &= (\epsilon + 2\kappa n_{th}) \delta(t - t'), \\ \langle :G_2(t) G_2(t') : \rangle &= (\epsilon - 2\kappa n_{th}) \delta(t - t'). \end{aligned} \quad (11)$$

式中 n_{th} 为热噪声的平均光子数. $K \neq 0$ 时, (10)式的解为

$$\begin{aligned}
b_j &= b_{j0} \exp(-\lambda_j t) + \frac{K}{\sqrt{2}} \left[\frac{b_{ji}(\omega)}{\lambda_j - i\omega} (\exp(-i\omega t) - \exp(-\lambda_j t)) \right. \\
&\quad \left. + \frac{b_{ji}(-\omega)}{\lambda_j + i\omega} (\exp(i\omega t) - \exp(-\lambda_j t)) \right] \\
&\quad + \int_{\Delta}^t \exp[-\lambda_j(t-\tau)] G_j(\tau) d\tau \quad j = 1, 2.
\end{aligned} \tag{12}$$

由此得出对易关系

$$\begin{aligned}
[b_2, b_1] &= [b_{20}, b_{10}] \exp[-(\lambda_1 + \lambda_2)t] + \frac{K^2}{2} [b_{2i}(\omega), b_{1i}(-\omega)] \\
&\quad \times \left(\frac{\exp(-i\omega t) - \exp(-\lambda_2 t)}{\lambda_2 - i\omega} \times \frac{\exp(i\omega t) - \exp(-\lambda_1 t)}{\lambda_1 + i\omega} \right) \\
&\quad + \frac{K^2}{2} [b_{2i}(-\omega), b_{1i}(\omega)] \\
&\quad \times \left(\frac{\exp(i\omega t) - \exp(-\lambda_2 t)}{\lambda_2 + i\omega} \times \frac{\exp(-i\omega t) - \exp(-\lambda_1 t)}{\lambda_1 - i\omega} \right) \\
&\quad + \int_0^t \int_0^t \exp[-\lambda_1(t-\tau') - \lambda_2(t-\tau)] [G_2(\tau), G_1(\tau')] d\tau d\tau'.
\end{aligned} \tag{13}$$

借助于(8)式,上式可写为

$$\begin{aligned}
1 &= \exp[-(\lambda_1 + \lambda_2)t] + \frac{K^2}{2} \left[\frac{\exp(-i\omega t) - \exp(-\lambda_2 t)}{\lambda_2 - i\omega} \right. \\
&\quad \times \frac{\exp(i\omega t) - \exp(-\lambda_1 t)}{\lambda_1 + i\omega} + \frac{\exp(i\omega t) - \exp(-\lambda_2 t)}{\lambda_2 + i\omega} \\
&\quad \left. \times \frac{\exp(-i\omega t) - \exp(-\lambda_1 t)}{\lambda_1 - i\omega} \right] \\
&\quad + \int_0^t \int_0^t \exp(-\lambda_1(t-\tau') - \lambda_2(t-\tau)) \langle [G_2(\tau), G_1(\tau')] \rangle d\tau d\tau'.
\end{aligned} \tag{13}'$$

由(13)'式解出

$$\begin{aligned}
\langle [G_2(\tau), G_1(\tau')] \rangle &= (2x - f(\tau)) \delta(\tau - \tau'), \\
f(\tau) &= \frac{K^2}{2} \exp[-(\lambda_1 + \lambda_2)\tau] \frac{d}{d\tau} \left(\frac{\exp(-i\omega\tau + \lambda_2\tau) - 1}{\lambda_2 - i\omega} \right. \\
&\quad \left. \times \frac{\exp(i\omega\tau + \lambda_1\tau) - 1}{\lambda_1 + i\omega} + \text{c.c.} \right).
\end{aligned} \tag{14}$$

参照(13)'式,若 t 很大,且 τ 趋近于 t , 于是(14)式可简化为

$$\begin{aligned}
f(\tau) &= 2xK^2 \frac{\lambda_1\lambda_2 + \omega^2}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)}, \\
[G_2(\tau), G_1(\tau')] &= 2x \left(1 - \frac{K^2(\lambda_1\lambda_2 + \omega^2)}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)} \right) \delta(\tau - \tau').
\end{aligned} \tag{15}$$

由(15)式明显看出注入相干光引起了 $G_1(\tau')$, $G_2(\tau)$ 满足的对易关系发生变化,相当于乘了一个因子 D . D 的定义如下:

$$D = 1 - \frac{K^2(\lambda_1\lambda_2 + \omega^2)}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)}. \tag{16}$$

这就相当于无规力乘了一个因子 $D^{1/2}$. 方程(11)可重写为

$$\langle :G_1(\tau)G_1(\tau') : \rangle = (\sigma + 2\chi n_{th})D\delta(\tau - \tau') \quad (17)$$

$$\langle :G_2(\tau)G_2(\tau') : \rangle = (\sigma - 2\chi n_{th})D\delta(\tau - \tau'). \quad (18)$$

注入率 K 的取值应受限于 D 取正值, 否则系统将是不稳定的. 亦即

$$K^2 \leq \frac{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)}{\chi^2 + \omega^2 - \sigma^2}. \quad (19)$$

当 $\omega = 0$, 即注入激光频率与泵浦光频率如相同, 由(18)式得

$$K^2 \leq \chi^2 - \sigma^2. \quad (20)$$

(20)式表明腔的损耗已部份被注入激光与增益所补偿. 如果等式成立便是完全补偿, 这时易于看出 $D = 0$, 即无规力消失.

现在讨论文献[5]的结果. 在文献[5]中假定无规力正比于注入激光 a_{in} , 并将 K 确认为 $\sqrt{2\gamma\delta\omega}$, 即 $\sqrt{2\chi\delta\omega}$, 并且是讨论连续谱 $\tilde{a}_{in}(\omega)$, 求出每一分量的贡献再积分. 故有

$$D = 1 - \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{2\chi(\chi^2 + \omega^2 - \sigma^2)}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)} d\omega = 0. \quad (21)$$

即无规力为零, 因为无规力的每一 Fourier 分量已经被当作“注入激光”计算. 当然也就不需另外引进无规力, 这就是(21)式表明的 $D = 0$. 但他并未真正计算注入激光. 所得结果, 腔内最大压缩为 2 倍, 与无激光情形相同^[13].

三、通过注入激光提高腔内参量放大光的压缩

现设 $\lambda t \gg 1$, 则方程(12)变为

$$\begin{aligned} b_j(\omega, t) &\simeq \frac{K}{\sqrt{2}} \left[\frac{b_{ji}(\omega)}{\lambda_j - i\omega} \exp(-i\omega t) + \frac{b_{ji}(-\omega)}{\lambda_j + i\omega} \right] \\ &\quad + \int_0^t \exp[-\lambda_j(t - \tau)] G_j(\tau) d\tau \\ &= b'_j + \int_0^t \exp[-\lambda_j(t - \tau)] G_j(\tau) d\tau \quad j = 1, 2. \end{aligned} \quad (22)$$

b_j 的方差可表示为(参照(17)式)

$$\begin{aligned} \langle :(\Delta b_1)^2 : \rangle &= \langle :(\Delta b'_1)^2 : \rangle + \frac{(\sigma + 2\chi n_{th})}{2\lambda_1} D, \\ \langle :(\Delta b_2)^2 : \rangle &= \langle :(\Delta b'_2)^2 : \rangle + \frac{(\sigma - 2\chi n_{th})}{2\lambda_2} D. \end{aligned} \quad (23)$$

现定义

$$\begin{aligned} a'(\omega) + a'^+(-\omega) &= \frac{K}{\lambda_1 - i\omega} (a_{in}(\omega) + a_{in}^+(-\omega)), \\ a'(\omega) - a'^+(-\omega) &= \frac{K}{\lambda_2 - i\omega} (a_{in}(\omega) - a_{in}^+(-\omega)). \end{aligned} \quad (24)$$

代入 b'_1, b'_2 的表式中, 便得

$$b'_1 = \frac{1}{2} [(a'(\omega) + a'^+(-\omega))\exp(-i\omega t) + (a'(-\omega) + a'^+(\omega))\exp(i\omega t)],$$

$$b'_2 = \frac{1}{2} [(a'(\omega) - a'^+(-\omega))\exp(i\omega t) + (a'(-\omega) - a'^+(\omega))\exp(i\omega t)]. \quad (25)$$

由方程(24),得到

$$a'(\omega) = \frac{K_1 + K_2}{2} a_{in}(\omega) + \frac{K_2 - K_1}{2} a_{in}^+(-\omega),$$

$$a'^+(-\omega) = \frac{K_2 - K_1}{2} a_{in}(\omega) + \frac{K_2 + K_1}{2} a_{in}^+(-\omega). \quad (26)$$

式中

$$K_1 = \frac{K}{\lambda_1 - i\omega}, \quad K_2 = \frac{K}{\lambda_2 - i\omega}.$$

采用记号 $\langle a, b \rangle = \langle ab \rangle - \langle a \rangle \langle b \rangle$, 可计算出

$$\langle a'(\omega), a'(-\omega) \rangle = \frac{K^2 \epsilon (x - i\omega)}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)},$$

$$\langle a^+(\omega), a'(\omega) \rangle = \frac{K^2 \epsilon^2}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)}, \quad (27)$$

于是由(25),(27)式便得

$$\langle :(\Delta b'_1)^2: \rangle = \langle :b'_1, b'_1: \rangle = \frac{K^2(x + \epsilon)\epsilon}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)},$$

$$\langle :(\Delta b'_2)^2: \rangle = \langle :b'_2, b'_2: \rangle = \frac{K^2(x - \epsilon)\epsilon}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)}. \quad (28)$$

注意到

$$X_1 = \frac{b_1}{\sqrt{2}}, \quad X_2 = \frac{b_2}{i\sqrt{2}},$$

$$a = X_1 + iX_2. \quad (29)$$

于是由方程(23),(28),(29),得

$$\langle :(\Delta X_1)^2: \rangle = \frac{1}{2} \left(\frac{K^2(x + \epsilon)\epsilon}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)} + \frac{\epsilon + 2xn_{th}}{2\lambda_1} D \right),$$

$$\langle :(\Delta X_2)^2: \rangle = \frac{-1}{2} \left(\frac{K^2(x - \epsilon)\epsilon}{(\lambda_1^2 + \omega^2)(\lambda_2^2 + \omega^2)} + \frac{\epsilon - 2xn_{th}}{2\lambda_2} D \right). \quad (30)$$

当 $K = 0$, 方程(30)给出

$$\langle :(\Delta X_1)^2: \rangle = \frac{\epsilon + 2xn_{th}}{4(x - \epsilon)},$$

$$\langle :(\Delta X_2)^2: \rangle = \frac{-\epsilon + 2xn_{th}}{4(x + \epsilon)}. \quad (31)$$

此即文献[10]的结果。若 $\omega = 0$, $n_{th} \simeq 0$, 且 $K^2 = E(x^2 - \epsilon^2)$, $E \leq 1$, 代入(30)式, 得

$$\langle :(\Delta x_2)^2: \rangle = -\frac{1}{4} \frac{\sigma(1+E)}{\lambda_2}. \quad (32)$$

调节注入率 K , 使得满足无规力消失条件, 亦即

$$K^2 = x^2 - \sigma^2. \quad (33)$$

又设腔的端面 A, B 的输出损耗分别为 x_1, x_2 , 参照图 1, 由 A 面注入, 于是有

$$x = x_1 + x_2, \quad K = x_1 \ll x. \quad (34)$$

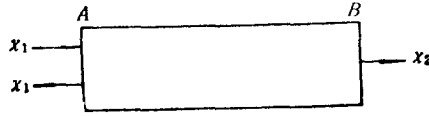


图 1

应用方程(33), (34), 得

$$\begin{aligned} \sigma &= \sqrt{x^2 - x_1^2} \simeq x - x_1^2/2x, \\ \langle (\Delta x_2)^2 \rangle &= \frac{1}{4} + \langle :(\Delta x_2)^2: \rangle \\ &= \frac{1}{4} \left(1 - \frac{2\sigma}{\sigma + x} \right) \simeq \frac{1}{16} \frac{x_1^4}{x^2}. \end{aligned} \quad (35)$$

故只要工作在阈值附近, $x \simeq \sigma$, $x_1 = \sqrt{x^2 - \sigma^2} \ll x$, 则腔内模式可达近乎理想压缩

$$\langle (\Delta x_2)^2 \rangle = \frac{1}{16} x_1^4/x^2 \simeq 0.$$

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ENHANCED SQUEEZING OF THE INTRACAVITY LIGHT FIELD PRODUCED IN PARAMETRIC AMPLIFICATION VIA LASER INJECTION

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ABSTRACT

For the squeezing of intracavity light fields produced in a parametric amplifier located within a cavity, we use laser injection which can compensate the effects of the cavity losses and therefore reduce the random force on the squeezing, and thus generate a large amount of intracavity squeezing near the threshold of oscillation.

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